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## **European Technical** Assessment

# English version prepared by ZAG

#### **General Part**

Technical Assessment Body issuing the **European Technical Assessment** 

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant(s)

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

ETA-18/0971 of 21.08.2019

ZAG Ljubljana

Sormat through bolts S-KA/ S-KAK/ S-KAH

33: Torque controlled expansion anchor of size M6 and M8 for multiple use for non-structural applications in concrete

**SORMAT OY** Harjutie 5 21290 RUSKO **Finland** 

www.sormat.com

Sormat Plant 1

14 pages including 11 annexes, which form an integral part of the document

EAD 330747-00-0601: Fasteners for use in concrete for redundant nonstructural systems, edition May 2018

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### Specific parts

#### 1 Technical description of the product

Sormat through bolts S-KA/ S-KAK/ S-KAH are made of zinc plated carbon steel (S-KA), hot dip galvanised carbon steel (S-KAK) or stainless steel (S-KAH). It consists of a bolt, expansion sleeve, hexagonal nut and washer.

Anchors are made in sizes M6 and M8. Anchor is placed into a drilled hole and anchored by torque-controlled expansion.

For the installed anchor see Figure given in Annex A1.

#### 2 Specification of the intended use(s) in accordance with the applicable **European Assessment Document (hereinafter EAD)**

The performances given in Chapter 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The provisions made in this European Technical Assessment are based on an assumed working life of the anchor of 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the manufacturer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

#### 3 Performance of the product and references to the methods used for its assessment

## 3.1 Mechanical resistance and stability (BWR 1)

The basic work requirements for mechanical resistance and stability are listed in Annexes C1 and C2.

#### 3.2 Safety in case of fire (BWR 2)

The basic work requirements for safety in case of fire are listed in Annexes C3 and C4.

#### 3.3 Hygiene, health and environment (BWR 3)

Regarding dangerous substances contained in this European Technical Assessment, there may be requirements applicable to the products falling within its scope (e.g. transported European legislation and national laws, regulations and administrative provisions). In order to meet provisions of the regulation (EU) No 305/2011, these requirements need also to be complied with, when they apply.

#### 3.4 Safety in use (BWR 4)

For basic work requirement safety in use the same criteria are valid as for basic work requirement mechanical resistance and stability.

#### 3.5 Protection against noise (BWR 5)

Not relevant.

#### 3.6 Energy economy and heat retention (BWR 6)

Not relevant.

#### 3.7 Sustainable use of natural resources (BWR 7)

No performance assessed.

#### 3.8 General aspects relating to fitness for use

Durability and serviceability are only ensured if specifications of intended use according Annex B1 are kept.

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4 Assessment and verification of constancy of performance (hereinafter AVCP) system applied, with reference to its legal base

According to the decision 96/582/EC of the European Commission<sup>1</sup> the system of assessment and verification of constancy of performance (see Annex V to regulation (EU) No 305/2011) 2+ apply.

5 Technical details necessary for the implementation of the AVCP system, as provided for on the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in Chapter 3 of EAD 330747-00-0601.

Issued in Ljubljana on 21. 08. 2019

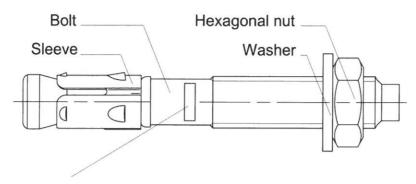
Signed by

Head of Service of TAB

Franc Capuder, M.Sc.

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## **SORMAT** through bolt



### Marking (Optional):

S-KA: S-KA: S-KA  $M.../t_{fix,max}$ 

S-KA M...× length

zinc platedzinc plated

S-KAK:

S-KAK M.../tfix,max

S-KAK M... × length

hot dip galvanizedhot dip galvanized

S-KAK: S-KAH:

S-KAH M.../t<sub>fix,max</sub>

- stainless steel A4

S-KAH:

S-KAH M... × length

- stainless steel A4

#### Examples:

S-KA 6/15

- zinc plated

S-KAK 6/15

hot dip galvanized

S-KAH 6/15 - stainless steel

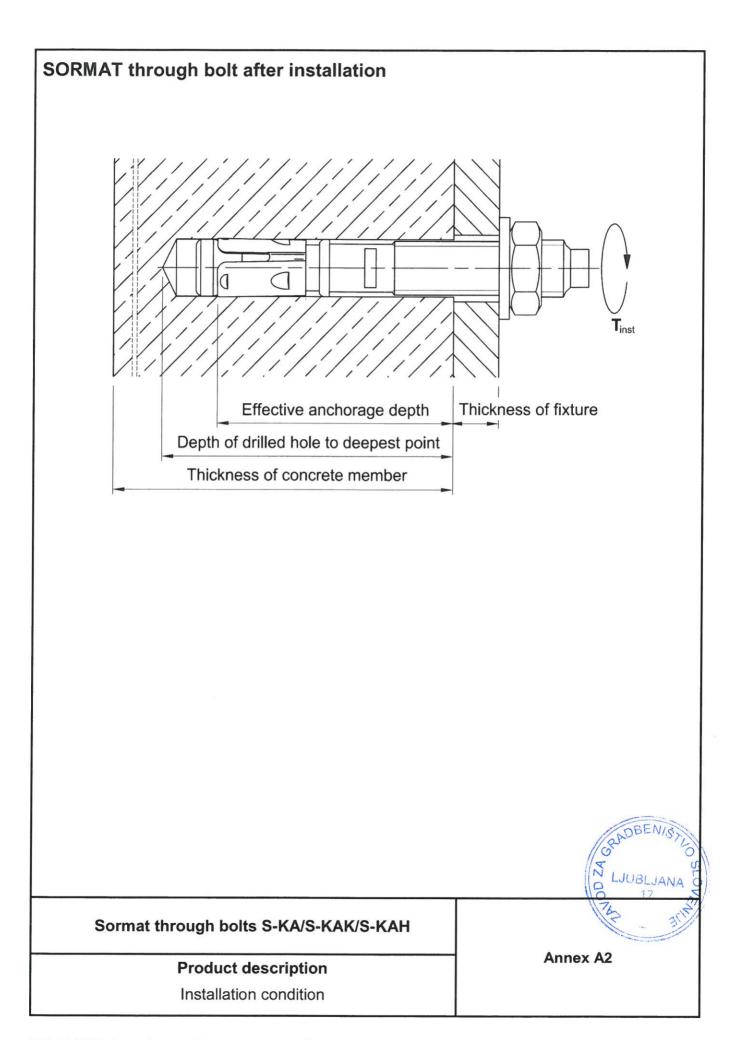
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Sormat through bolts S-KA/S-KAK/S-KAH

**Product description** 

**Product** 

Annex A1



## **SORMAT** through bolt

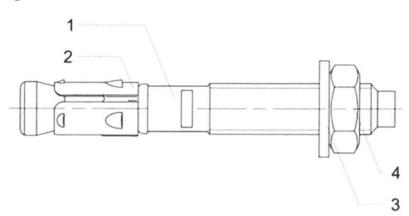


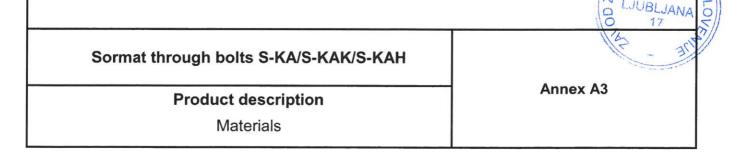
Table A1: Materials for S-KA and S-KAK

Part	Designation	Material 1) 2)
1	Bolt	Cold forged steel
2	Sleeve	Cold rolled galvanized steel strip, EN 10346
3	Washer	Steel, DIN 125 (EN ISO 7089), DIN 440 (EN ISO 7094), DIN 9021 (EN ISO 7093)
4	Hexagonal nut	Steel, property class 8, DIN 934 (EN ISO 4032)

 $<sup>^{1)}</sup>$ S-KA: Parts 1,3 and 4 are zinc electroplated according to EN ISO 4042 ≥ 5μm and bright passivated  $^{2)}$ S-KAK: Parts 1,3 and 4 are hot dip galvanized according to EN ISO 10684, EN ISO 1461

Table A2: Materials for S-KAH

Part	Designation	Material
1	Bolt	Stainless steel, EN 10088-3
2	Sleeve	Stainless steel strip, EN 10088-2
3	Washer	Stainless steel, DIN 125 (EN ISO 7089), DIN 440 (EN ISO 7094), DIN 9021 (EN ISO 7093)
4	Hexagonal nut	Stainless steel, property class 80, DIN 934 (EN ISO 4032)



### Specifications of intended use

#### Anchorages subjected to:

- Static, quasi static load.
- Use only for multiple use for non-structural applications according to EAD 330747-00-0601
- Fire exposure.

#### Base materials:

- Cracked and non-cracked concrete.
- Reinforced and unreinforced normal weight concrete of strength class C20/25 at minimum and C50/60 at maximum according to EN 206:2013A1:2016.

#### Use conditions (Environmental conditions):

- The S-KA and S-KAK and S-KAH M6-1 anchors may be used in concrete subject to dry internal conditions.
- The S-KAH M6-2 and S-KAH M8 anchors may be used in concrete subject to dry internal conditions and also in concrete subject to external atmospheric exposure (including industrial and marine environment), or exposure in permanently damp internal conditions, if no particular aggressive conditions exist.

Note: Particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e.g. desulphurization plants or road tunnels where de-icing materials are used).

#### Design:

- Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- Anchorages under static and quasi-static actions are designed in accordance with EOTA TR 055, Edition December 2016, Amended February 2018 or EN 1992-4:2018.
- For application with resistance under fire exposure the anchorages are designed in accordance with the method given in EOTA TR 020, Edition May 2004.
- Verifiable calculation notes and drawings are prepared taking into account of the load to be anchored. The position of the anchor is indicated on the design drawings (e.g. position of the anchor relative to reinforcement or to supports, etc.).

#### Installation:

- Anchor installation carried out by appropriately qualified personnel and under the supervision of the person responsible for technical matters on the site.
- Use of the anchor only as supplied by the manufacturer without exchanging the components of an anchor.
- Anchor installation in accordance with the manufacturer's specifications and drawings using the appropriate tools.
- Checks before placing the anchor to ensure that the strength class of the concrete in which the
  anchor is to be placed is in the range given and is not lower that of the concrete to which the
  characteristic loads apply for.
- Check of concrete being well compacted, e.g. without significant voids.
- Cleaning of the hole of drilling dust.
- Anchor installation ensuring the specified embedment depth.
- Keeping of the edge distance and spacing to the specified values without minus tolerances.
- In case of aborted hole, drilling of new hole at a minimum distance of twice the depth of the aborted hole, or smaller distance provided the aborted drill hole is filled with high strength non-shrinkage mortar. No shear or oblique tension loads are allowed in the direction of a not filled aborted hole.
- Application of the torque moment given in Annex B3 using a calibrated torque wrench./

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Sormat through bolts S-KA/S-KAK/S-KAH	Tat and
Intended use	Annex B1
Specifications	

## **SORMAT** through bolt

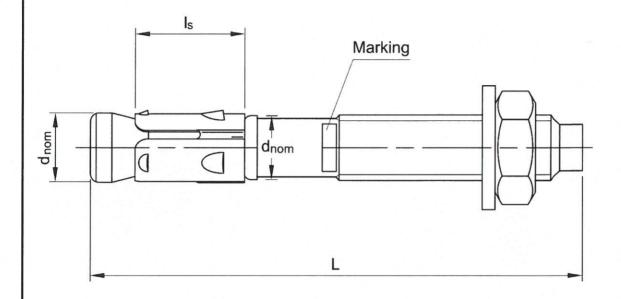


Table B1: Dimension of an anchor

Size	Nominal diameter d <sub>nom</sub> [mm]	Sleeve length l <sub>s</sub> [mm]	Total length L [mm]
M6	6	14,5	38 420
M8	8	15,9	50 420

Sormat through bolts S-KA/S-KAK/S-KAH

Intended use

Anchor dimensions

Annex B2

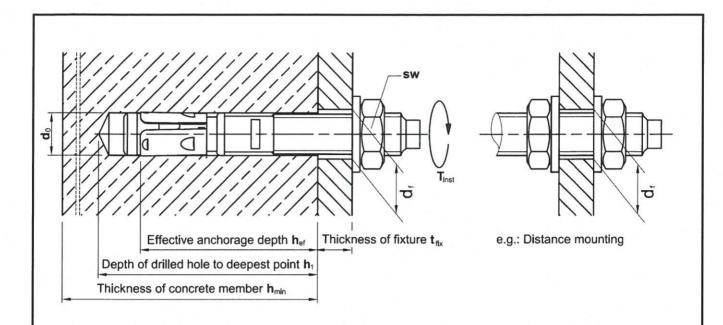


Table B2: Installation data

	Anchor size					
Sormat thi	M6-1	M6-2	M8			
Drill hole diameter	d <sub>0</sub>	[mm]	6	6	8	
Cutting diameter at the upper tolerance limit (maximum diameter bit)		d <sub>cut,max</sub> ≤	[mm]	6,40	6,40	8,45
Depth of drilled hole to deepest point		h <sub>1</sub> ≥	[mm]	35	45	45
Effective anchorage depth		h <sub>ef</sub>	[mm]	25	35	35
Diameter of clearance hole in the fixture		d <sub>f</sub> ≤	[mm]	7	7	9
Thickness of the fixtu	re	t <sub>fix,max</sub>	[mm]	380	370	370
Width across flats		SW	[mm]	10	10	13
Required torque	S-KA			4	7	11
	S-KAK	T <sub>inst</sub>	[Nm]	4	7	15
	S-KAH	MACO SAL		5	8	15

Sormat through bolts S-KA/S-KAK/S-KAH

Intended use
Installation data

Table B3: Minimum thickness of concrete member, spacing and edge distance

Sormat through bolts S-KA/S-K	Anchor size				
Somat tillough boils 3-KA/3-K	M6-1	M6-2	M8		
Minimum thickness of concrete member	h <sub>min</sub>	[mm]	80	80	80
Minimum spacing	S <sub>min</sub>	[mm]	50	40	60
Minimum edge distance	C <sub>min</sub>	[mm]	50	40	60

Sormat through bolts S-KA/S-KAK/S-KAH

Intended use

Installation data

Annex B4

**Table C1:** Characteristic resistances under tension loads in case of static and quasi-static loading for design according EOTA TR 055 or EN 1992-4:2018

0	- K- O KAKO KAK	10 14 4 1 1			Anchor size	
Sormat through	bolts S-KA/S-KAK	/S-KAH		M6-1	M6-2	М8
Steel failure						
01	S-KA/S-KAK			8,6		14,8
Characteristic resistance	S-KAH	$ N_{Rk,s}$	[kN]	9,	9	15,8
Partial safety factor		γ <sub>Ms</sub> 2)	[-]		1,4	
Pull-out failure						
Characteristic resistance in cracked and non-cracked		I N	FI . 17	2,0	3,5	7,0
concrete C20/25	S-KAH	N <sub>Rk,p</sub>	[kN]	3,0	5,0	7,0
			C25/30	1,12	1,12	1,08
		C30/37	1,22	1,22	1,15	
Increasing factor for N		Ψ <sub>c</sub>	C35/45	1,32	1,32	1,20
ncreasing factor for N <sub>Rk,p</sub>		₩°C	C40/50	1,41	1,41	1,26
			C45/55	1,50	1,50	1,32
			C50/60	1,58	1,58	1,44
Destinia for the form			[-]	1,0		
Partial safety factor		γ <sub>inst</sub> 2) γ <sub>Mp</sub> 3)	[-]	1,5 <sup>3)</sup>		
Concrete cone and splitting	failure					
Effective anchorage depth		h <sub>ef</sub>	[mm]	25	35	35
Factor for cracked concrete		k <sub>cr</sub>	[-]	7,7		
Factor for non-cracked concre	te	k <sub>ucr</sub>	[-]	11,0		
Spacing		S <sub>cr,N</sub>	[mm]	75	105	105
Edge distance		C <sub>cr,N</sub>	[mm]	37,5	52,5	52,5
Spacing ( splitting )		S <sub>cr,sp</sub>	[mm]	140	120	120
Edge distance (splitting)		C <sub>cr,sp</sub>	[mm]	70	60	60
Partial safety factor		γ <sub>Msp</sub> 2)	[-]		1,5	

# Sormat through bolts S-KA/S-KAK/S-KAH Annex C1 **Performance** Characteristic resistance under tension loads

<sup>&</sup>lt;sup>1)</sup> Pull-out failure is not decisive <sup>2)</sup> In absence of other national regulations <sup>3)</sup> The installation safety factor of  $\gamma_2$  = 1,0 is included

**Table C2:** Characteristic resistances under shear loads in case of static and quasi-static loading for design according to EOTA TR 055 or EN 1992-4:2018

Sormat through bolts S-KA/S-KAK/S-KAH			-	Anchor size		
Sormai	through boits 5-KA/5-KAK	/S-KAH		M6-1	M6-2	M8
Steel failure witho	ut lever arm					
Characteristic	S-KA/S-KAK	.,	F1 A 17	1	4,3	10,0
resistance	S-KAH	V <sub>Rk,s</sub>	[kN]	1	4,3 12 1,25 1	13,4
Partial safety factor		γ <sub>Ms</sub> 1)	[-]		1,25	
Factor for considering	ng ductility	k <sub>7</sub>	[-]		1	
Steel failure with le	ever arm					
Characteristic S-KA/S-KAK		1.40		7	•	20
	S-KAH	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	9	/ 12 1,25 1 7 9 1,25 1 1 1 1,5	22
Partial safety factor		γ <sub>Ms</sub> 1)	[-]	1,25		
Concrete pryout fa	ilure					
k-factor		k <sub>8</sub>	[-]	1	1	1
Partial safety factor		γ <sub>Mc</sub> 1)	[-]	1,5		
Concrete edge fail	ure					
Effective length of a	nchor under shear load	l <sub>f</sub>	[mm]	25	35	35
Outside diameter of	anchor	d <sub>nom</sub>	[mm]	6	6	8
Uncracked and cra edge reinforcement	icked concrete without any				1,0	
Cracked concrete v reinforcement > Ø12		$\Psi_{\text{re,V}}$	[-]		1,2	
Uncracked or cracked concrete with edge reinforcement and closely spaced stirrups (a ≤ 100mm and a ≤ 2c₁)					1,4	
Partial safety factor		γ <sub>Mc</sub> 1)	[-]		1,5	

<sup>1)</sup> In absence of other national regulations

Sormat through bolts S-KA/S-KAK/S-KAH

Performance

Characteristic resistance under shear loads

**Table C3:** Characteristic resistances under tension loads in case of fire exposure for design according to EOTA TR 020 or EN 1992-4:2018

Sormat thro	ugh bolts S-KA	S-KAKIS	S-KAH		Anchor size			
oomat tiilo	agii boits o-tta	JO-KARV	J-KAII	M6-1	M6-2	M8		
Steel failure								
		R30	[kN]	1	0,16	0,26		
	S-KA/S-KAK	R60	[kN]	1	0,14	0,24		
	3-KA/3-KAK	R90	[kN]	1	0,11	0,18		
Characteristic resistance		R120	[kN]	1	0,08	0,13		
N <sub>Rk,s,fi</sub>		R30	[kN]	1	0,16	0,53		
111,0,11	S-KAH	R60	[kN]	1	0,14	0,42		
	3-KAH	R90	[kN]	1	0,11	0,32		
		R120	[kN]	1	0,08	0,26		
Pull-out failur	е							
	S-KA/S-KAK	R30	[kN]	0,50	0,50	1,75		
		R60	[kN]	0,50	0,50	1,75		
		R90	[kN]	0,50	0,50	1,75		
Characteristic		R120	[kN]	0,40	0,40	1,40		
resistance N <sub>Rk,p,fi</sub>	S-KAH	R30	[kN]	0,75	0,75	1,63		
(KK, P, II		R60	[kN]	0,75	0,75	1,63		
		R90	[kN]	0,75	0,75	1,63		
		R120	[kN]	0,60	0,60	1,30		
Concrete con	and splitting	failure 1)						
		R30	[kN]	0,56	1,30	1,30		
Characteristic i	esistance	R60	[kN]	0,56	1,30	1,30		
N <sup>0</sup> <sub>Rk,c,fi</sub>		R90	[kN]	0,56	1,30	1,30		
	10 m	R120	[kN]	0,45	1,04	1,04		
Spacing		S <sub>cr,N,fi</sub>	[mm]		4 x h <sub>ef</sub>			
Spacing		S <sub>min</sub>	[mm]	50	40	60		
		C <sub>cr,N,fi</sub>	[mm]		2 x h <sub>ef</sub>			
Edge distance				Fire attack f	rom one side: c <sub>r</sub>	<sub>nin</sub> = 2 x h <sub>ef</sub>		
	Edge distance		[mm]	Fire attack from more than one side: $c_{min} \ge 300 \text{ mm}$ and $\ge 2 \times h_{ef}$				

As a rule, splitting failure can be neglected when cracked concrete and reinforcement is assumed Design under fire exposure is performed according to the design method given in EOTA TR 020. Under fire exposure usually cracked concrete is assumed. The design equations are given in EOTA TR 020 § 2.2.1.

In the absence of other national regulations the partial safety factor for resistance under fire exposure  $\gamma_{M,fi} = 1,0$  is recommended.

### Sormat through bolts S-KA/S-KAK/S-KAH

**Performance** 

Characteristic tension resistance under fire exposure

Annex C3

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**Table C4:** Characteristic resistances under shear loads in case of fire exposure for design according to EOTA TR 020 or EN 1992-4:2018

Sormat thro	ugh bolts S-KA	IS-KAKIS	-KVH	Anchor size		
Somat timo	ugii boits 3-KA	JO-NAN/S	-KAN	M6-1	M6-2	M8
Steel failure w	vithout lever an	m				
		R30	[kN]	1	0,16	0,26
	S-KA/S-KAK	R60	[kN]	1	0,14	0,24
	S-NA/S-NAN	R90	[kN]	1	0,11	0,18
Characteristic resistance		R120	[kN]	1	0,08	0,13
V <sub>Rk,s,fi</sub>		R30	[kN]	1	0,16	0,53
IN,O,II	S-KAH	R60	[kN]	1	0,14	0,42
	3-NAIT	R90	[kN]	1	0,11	0,32
		R120	[kN]	1	0,08	0,26
Steel failure w	ith lever arm					
	S-KA/S-KAK	R30	[kN]	1	0,15	0,37
		R60	[kN]	1	0,14	0,34
		R90	[kN]	1	0,11	0,26
Characteristic resistance		R120	[kN]	1	0,08	0,19
M <sup>0</sup> <sub>Rk,s,fi</sub>		R30	[kN]	1	0,15	0,75
130,3,11	S-KAH	R60	[kN]	1	0,14	0,60
	3-KAN	R90	[kN]	1	0,11	0,40
		R120	[kN]	1	0,08	0,37
Concrete pryd	out failure					
k-factor		k <sub>8</sub>	[-]	1	1	1
		R30	[kN]	0,56	1,30	1,30
Characteristic r	resistance	R60	[kN]	0,56	1,30	1,30
$V_{Rk,cp,fi}$		R90	[kN]	0,56	1,30	1,30
		R120	[kN]	0,45	1,04	1,04

#### Concrete edge failure

The initial value  $V_{Rk,c,fi}^0$  of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:

 $V^0_{Rk,c,fi} = 0.25 \times V^0_{Rk,c} \ (\le R90)$   $V^0_{Rk,c,fi} = 0.20 \times V^0_{Rk,c} \ (R120)$  with  $V^0_{Rk,c}$  initial value of the characteristic resistance in cracked concrete C20/25 under normal temperature.

Design under fire exposure is performed according to the design method given in EOTA TR 020.

Under fire exposure usually cracked concrete is assumed. The design equations are given in EOTA TR 020 § 2.2.1.

EOTA TR 020 covers design for fire exposure from one side. For fire attack from more than one side the edge distance must be increased to  $c_{min} \ge 300$  mm and  $\ge 2 \text{ x h}_{ef}$ .

In the absence of other national regulations the partial safety factor for resistance under fire exposure  $\gamma_{M,fi} = 1,0$  is recommended.

#### Sormat through bolts S-KA/S-KAK/S-KAH

#### **Performance**

Characteristic shear resistance under fire exposure

Annex C4